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SUBJECT:	Fuel Cycle Costs in a Graphite Moderated Slightly Enriched Fused Salt Reactor	y	
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FROM:	C. E. Guthrie		

Abstract

A fuel cycle economic study has been made for a $315 \ Mw_e$ graphite moderated slightly enriched molten salt fueled reactor. Fuel cycle costs in the order of $3.3 \ mills/kwh$ were calculated for the throw-away cycle. Recovery of the uranium and plutonium at the end of the cycle reduces the cycle costs to $\sim 1.6 \ mills/kwh$. Changes in the waste storage and reprocessing costs have a relatively minor effect on fuel cycle costs.

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Foreword

This revision incorporates more accurate nuclear calculations and some changes in economic basis.

Introduction

One potential advantage of a fluid fueled reactor is a low fuel cycle cost. There are two alternate approaches, both unique to the fluid fuel concepts, one might take to realize this potential: (1) continuous reprocessing, thereby keeping the poisons at a minimum and the conversion (or breeding) ratio at a maximum, or (2) continuous additions of enriched fuel (to make up for burnout and reactivity decrease), thereby attaining very high burnup on the original fuel charge. The latter approach is the one more applicable to the fused salt (LiF, BeF, UF₄) reactor operating on the $U^{235}-U^{238}$ cycle. For fused salt reactors operating on the Th-U cycle either approach can be used since the volatility process could be used to continuously (or semicontinuously) recover the U-235 and U-233.

This study has been made to determine the range of fuel cycle costs anticipated for a graphite moderated fused salt burner reactor operating on the $U^{235}-U^{238}$ cycle. The nuclear calculations and cycle costs for the Th- U^{235} cycle will be worked out and reported at a later date.

Reactor Basis*

The reactor considered is graphite moderated with a fluid fuel consisting of a molten mixture of lithium-7 fluoride, beryllium fluoride and slightly enriched uranium fluoride. During the reactor cycle highly enriched UF_{l_1} is added to the system to supply burnup and make up for the reactivity loss due to accumulated fission products. The inventory of fissile isotopes in the reactor and the U-235 additions as a function of time are shown in Figs. 1 and 2, respectively. The other reactor parameters are:

> 775 Mw Thermal 315 Mw Electrical 900 ft³ Fused Salt Inventory 80% Load Factor 1.4% Initial U-235 Enrichment 20% UF₁ Salt Composition, Mole % 70% Li⁷F 10% BeF₂

*All reactor data supplied by L. G. Alexander from ORACLE calculations.





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Economic Basis

Two fuel cycle cases have been considered, both of which assume no Li-7 recovery. In each case the cycle repeats by the reactor being fueled with fresh salt containing 1.4% enriched U.

1) Throw-away cycle - At the end of the reactor cycle (or lifetime) the reactor salt inventory including fissionable isotopes would be discarded into on-site waste tanks for permanent storage. A \$1,000,000 investment has been assumed at the end of the cycle for a storage facility and provision for permanent monitoring.

2) U and Pu recovered at end of cycle by solvent extraction - Recovery costs of \$150/kg U (representative of current technology and scale of processing) and \$50/kg U (large scale technology) have been estimated.

The economics were calculated on the following basis:

a 10% return (before taxes).

Salt cost \$1700/ft³ (excluding U value).
U value at official price schedule.
Pu credit \$15/gm of Pu-239 and Pu-241.
4% use charge was paid on initial loading of U, U-235 added during cycle, and Pu buildup during the cycle.
A 5% interest sinking fund was used to pay for either U discard and storage costs or processing costs at the end of the cycle and to take care of increasing use charges.
The investment in salt was payed off over the cycle with

Results

The fuel cycle costs, claculated for each case as a function of cycle time, are shown in Fig. 3. A minimum fuel cycle cost of 1.6 mills/kwh is predicted for a reactor cycle of 4.5 years when the U and Pu are recovered at the end of the cycle for \$50/kg U. For \$150/kg U recovery costs, cycle costs are essentially constant at ~2 mills/kwh for cycles in excess of 5 years. In all cases it pays to recover the U and Pu at the end of the cycle since the minimum throw-away cycle cost is 3.35 mills/kwh. Table I shows a breakdown of the costs for the five-year cycle.

Errors in the fused salt waste disposal and initial salt costs have little effect on the fuel cycle costs for cycles 5 years or longer. Increasing the waste disposal cost by 1,000,000/cycle and the salt cost by $1000/ft^3$ would increase the five-year cycle costs by 0.08 mill/kwh and 0.12 mill/kwh respectively. Changing the return on salt investment to 12% and the interest on sinking fund to 6% (instead of 10% and 5%) would decrease

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Fig. 3. Fuel Cycle Cost vs. Cycle Time

Table I

Five-Year Cycle Cost Breakdown

	Throwaway	Recovery Cycle		
	Cycle	\$50/kg U	\$150/kg U	
Use Charge on Initial U Loading Use Charge on U-235 Added and	0.13 Mills/kwh	0.13 Mills/kwh	0.13 Mills/kwh	
Pu Buildup	0.29	0.29	0.29	
Salt Amortization	0.21	0.21	0.21	
Burnup	0.79	0.79	0.79	
Fuel Throwaway Cost	1.84	-	-	
Waste Storage for Throwaway	0.08	-	- .	
Reprocessing Charges		0.23	0.69	
Total Cycle Costs	3.34 Mills/kwh	1.65 Mills/kwh	2.11 Mills/kwh	

the cycle cost by 0.01 mill/kwh for the 5-year cycle and by 0.15 mill/kwh for the ll-year cycle.

It is interesting to compare these fuel cycle costs, which are for a single reactor with present reprocessing technology, with the fuel cycle costs anticipated for solid fueled reactors at the present time. Two such reactors which are typical are the Yankee with a 7.1 mills/kwh(1) fuel cost and the Indian Point with a 5.8 mills/kwh⁽²⁾ fuel cost. These costs will be reduced by the mass production of fuel elements and large scale reprocessing possible in a large nuclear economy. It will probably take, however, a nuclear economy in the order of 10^5 Mw_{e} (1980-2000) to reduce solid fueled reactor fuel cycle costs to 1.5 mills/kwh. As far as fuel cycle costs are concerned slightly enriched fused salt reactors appear to be superior at present and competitive in the future to heterogeneous reactors.

⁽¹⁾ Schoupp, W. E., Advanced Pressurized Water Systems Proceedings of Atomic Energy Management Conference, March 17-19, 1958, Chicago, Ill., p. 142.

 ⁽²⁾ J. F. Fairman, Estimated Costs of Indian Point Nuclear Power Plant, Ibid,
 p. 357.

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